Regulations Compliance Report



Approved Document L1A 2010 edition assessed by Stroma FSAP 2009 program, Version: 1.5.0.85 Printed on 17 April 2015 at 14:39:23

Project Information:

Assessed By: Aymon Winter (STRO014511) **Building Type:** Flat

Dwelling Details:

NEW DWELLING DESIGN STAGE

Site Reference: Lancaster Street Plot Reference: 07-14-40586 B17 PL1

Flat B17 Address:

Client Details:

H G Construction Ltd - Hitchin Name: 4 Hunting Gate, Hitchin, SG40TJ Address:

This report covers items included within the SAP calculations.

It is not a complete report of regulations compliance.

1 TER and DER

Fuel for main heating system: Mains gas (c), Mains gas (c)

Fuel factor: 1.00 (mains gas (c), mains gas (c))

Target Carbon Dioxide Emission Rate (TER) 15.98 kg/m²

Dwelling Carbon Dioxide Emission Rate (DER) 11.84 kg/m² OK

2 Fabric U-values

Element Highest Average 0.15 (max. 0.30) OK External wall 0.16 (max. 0.70) Party wall 0.00 (max. 0.20) **OK** (no floor) Floor Roof (no roof)

OK **Openings** 1.60 (max. 2.00) 1.60 (max. 3.30)

3 Air permeability

6.00 Air permeability at 50 pascals **OK** Maximum 10.0

4 Heating efficiency

Main Heating system: Community heating schemes - mains gas

Secondary heating system: None

5 Cylinder insulation

Hot water Storage: No cylinder

6 Controls

Space heating controls Charging system linked to use of community heating, programmer and TRVs OK

Hot water controls: No cylinder

7 Low energy lights

Percentage of fixed lights with low-energy fittings 100.0%

75.0% **OK** Minimum

8 Mechanical ventilation

Not applicable

Regulations Compliance Report



9 Summertime temperature

Overheating risk (Thames valley):

Based on:

Overshading:

Windows facing: North East Windows facing: North West

Ventilation rate:

Blinds/curtains:

Medium

OK

Average or unknown

20.3m², Overhang twice as wide as window, ratio NaN 4.55m², Overhang twice as wide as window, ratio NaN

4.00

Light-coloured curtain or roller blind shutter closed 100% of daylight hours

10 Key features

External Walls U-value External Walls U-value External Walls U-value

Community heating, heat from boilers - mains gas

Photovaltaic array

0.13 W/m²K

0.12 W/m²K

0.16 W/m²K

SAP Input



Property Details: 07-14-40586 B17 PL1

Address: Flat B17
Located in: England
Region: Thames valley

UPRN:

Date of assessment: 16 April 2015 Date of certificate: 17 April 2015

Assessment type: New dwelling design stage

Transaction type:

Tenure type:

Related party disclosure:

Thermal Mass Parameter:

New dwelling
Unknown
No related party
Indicative Value Low

Dwelling designed to use less than 125 litres per Person per day: True

Property description:

Dwelling type:

Flat

Detachment:

Year Completed:

2015

Floor Location:

.

Floor 0

Floor area:

IE m2

30.9 m² (fraction 0.356)

Storey height:

86.7

86.75 m²

2.56 m

Living area: Front of dwelling faces:

South West

Opening types:

| Name: | Source: | Type: | Glazing: | Argon: | Frame: |
|------------|--------------|---------|--------------------------------|--------|--------|
| Front Door | Manufacturer | Solid | | | PVC-U |
| Rear Elev | Manufacturer | Windows | low-E, $En = 0.05$, soft coat | Yes | Metal |
| Side Elev | Manufacturer | Windows | low-E, $En = 0.05$, soft coat | Yes | Metal |

| Name: | Gap: | Frame Fa | actor: g-value: | U-value: | Area: | No. of Openings: |
|------------|--------------|----------|-----------------|----------|-------|------------------|
| Front Door | mm | 0.7 | 0 | 1.6 | 2.12 | 1 |
| Rear Elev | 16mm or more | 0.8 | 0.63 | 1.6 | 20.3 | 1 |
| Side Elev | 16mm or more | 0.8 | 0.63 | 1.6 | 4.55 | 1 |

| Name: | Type-Name: | Location: | Orient: | Width: | Height: |
|------------|------------|---------------------|------------|--------|---------|
| Front Door | | Walls to Corridor | South West | 0 | 0 |
| Rear Elev | | Block External Wall | North East | 0 | 0 |
| Side Elev | | Block External Wall | North West | 0 | 0 |

Overshading: Average or unknown

Opaque Elements

| Type: | Gross area: | Openings: | Net area: | U-value: | Ru value: | Curtain wall: | Карра: |
|--------------------|-------------|-----------|-----------|----------|-----------|---------------|--------|
| External Element | <u>ts</u> | | | | | | |
| Walls to Corridor | 31.54 | 2.12 | 29.42 | 0.14 | 0.43 | False | N/A |
| Walls to Stairwell | 2.28 | 0 | 2.28 | 0.14 | 0.9 | False | N/A |
| Block External Wal | I 58.57 | 24.85 | 33.72 | 0.16 | 0 | False | N/A |
| Internal Element | <u>s</u> | | | | | | |
| Party Elements | | | | | | | |
| Party Walls | 26.02 | | | | | | N/A |
| Party Ceiling | 86.75 | | | | | | N/A |
| Party Ceiling | 86.75 | | | | | | N/A |

Thermal bridges

Thermal bridges: No information on thermal bridging (y=0.15) (y=0.15)

SAP Input



Ventilation:

Pressure test: Yes (As designed)

Ventilation: Natural ventilation (extract fans)

Number of chimneys: 0
Number of open flues: 0
Number of fans: 3
Number of sides sheltered: 2
Pressure test: 6

Main heating system

Main heating system: Community heating schemes

Heat source: Community CHP

heat from boilers - mains gas, heat fraction 0.6, efficiency 83.9

Heat source: Community boilers

heat from boilers – mains gas, heat fraction 0.4, efficiency 92

Piping>=1991, pre-insulated, low temp, variable flow

Main heating Control:

Main heating Control: Charging system linked to use of community heating, programmer and TRVs

Control code: 2306

Secondary heating system:

Secondary heating system: None

Water heating:

Water heating: From main heating system

Water code: 901

Fuel :heat from boilers - mains gas

No hot water cylinder Solar panel: False

Others:

Electricity tariff: standard tariff
In Smoke Control Area: Unknown
Conservatory: No conservatory

Low energy lights: 100%
Terrain type: Dense urban
EPC language: English
Wind turbine: No

Photovoltaics: <u>Photovoltaic 1</u>

Installed Peak power: 0.19 Tilt of collector: 30°

Overshading: None or very little Collector Orientation: South East

Assess Zero Carbon Home: No



User Details: Aymon Winter STRO014511 **Assessor Name:** Stroma Number: Stroma FSAP 2009 **Software Version: Software Name:** Version: 1.5.0.85 Property Address: 07-14-40586 B17 PL1 Flat B17 Address: 1. Overall dwelling dimensions: Ave Height(m) Area(m²) Volume(m³) Ground floor 86.75 (1a) x (3a) 2.56 (2a) 222.08 Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+....(1n)(4)86.75 Dwelling volume (3a)+(3b)+(3c)+(3d)+(3e)+....(3n) =222.08 (5) total main Secondary other m³ per hour heating heating x 40 =Number of chimneys (6a) 0 0 x 20 =Number of open flues 0 O O 0 0 (6b) Number of intermittent fans x 10 =(7a) 3 30 x 10 =Number of passive vents (7b) 0 0 x 40 =Number of flueless gas fires (7c)Air changes per hour Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = \div (5) = (8) 0.14 If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16) Number of storeys in the dwelling (ns) (9)O Additional infiltration (10)[(9)-1]x0.1 =0 Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction (11)0 if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35 If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0 0 (12) If no draught lobby, enter 0.05, else enter 0 (13)0 Percentage of windows and doors draught stripped (14)0 Window infiltration $0.25 - [0.2 \times (14) \div 100] =$ 0 (15)Infiltration rate (8) + (10) + (11) + (12) + (13) + (15) =O (16)Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area (17)6 If based on air permeability value, then $(18) = [(17) \div 20] + (8)$, otherwise (18) = (16)0.44 (18)Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used Number of sides on which sheltered (19)2 $(20) = 1 - [0.075 \times (19)] =$ Shelter factor (20)0.85 $(21) = (18) \times (20) =$ Infiltration rate incorporating shelter factor (21)0.37 Infiltration rate modified for monthly wind speed Feb Sep Jan Mar Apr Mav Jun Jul Aug Oct Nov Dec Monthly average wind speed from Table 7 (22)m =5.1 4.5 4.1 3.9 3.7 3.7 4.2 4.5 4.8 5.1

1.12

1.02

0.98

0.92

0.92

1.05

1.12

1.2

1.27

1.27

Wind Factor $(22a)m = (22)m \div 4$

1.27

1.35

(22a)m



| Adjusted infiltra | ation rate | e (allowi | ng for sh | elter an | d wind s | speed) = | (21a) x | (22a)m | | | | | |
|--|-----------------|-----------|-------------|------------|----------------|-----------------|----------------|--|-------------------|---------------------------|--------------------|------------|---------------|
| 0.5 | 0.47 | 0.47 | 0.42 | 0.38 | 0.36 | 0.34 | 0.34 | 0.39 | 0.42 | 0.44 | 0.47 | | |
| Calculate effec | | • | rate for ti | ne appli | cable ca | se | ! | ! | | | ! | • | (cc.) |
| If mechanica | | | andiv N (2º | 3h) - (23a |) × Fmv (e | aguation (N | NSN othe | rwisa (23h |) <i>- (</i> 23a) | | | 0 | (23a) |
| If balanced with | | | | | | | | |) = (23a) | | | 0 | (23b) |
| a) If balance | | - | | _ | | | | | 2h\m + (' | 23h) ~ [⁴ | 1 _ (23c) | · 1001 | (23c) |
| (24a)m= 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | + 100j | (24a) |
| b) If balance | | | | | | <u> </u> | | | | | | | , , |
| (24b)m= 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (24b) |
| c) If whole h | ouse ext | ract ven | tilation o | r positiv | e input v | L ventilatio | n from o | L outside | | | ļ | l | |
| if (22b)m | | | | • | • | | | | 5 × (23b |) | | | |
| (24c)m= 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (24c) |
| d) If natural v | | | | | • | | | | | | - | | |
| if (22b)m | | <u> </u> | <u> </u> | • | <u> </u> | | | | | | | Ī | (244) |
| (24d)m= 0.62 | 0.61 | 0.61 | 0.59 | 0.57 | 0.56 | 0.56 | 0.56 | 0.58 | 0.59 | 0.6 | 0.61 | | (24d) |
| Effective air | | | <u> </u> | • | `` | ŕ | | ` | 0.50 | 0.6 | 0.64 | 1 | (25) |
| (25)m= 0.62 | 0.61 | 0.61 | 0.59 | 0.57 | 0.56 | 0.56 | 0.56 | 0.58 | 0.59 | 0.6 | 0.61 | | (25) |
| 3. Heat losses | s and hea | at loss p | paramete | er: | | | | | | | | | |
| ELEMENT | Gross area (| - | Openin | | Net Ar A ,r | | U-valı W/m2 | | A X U (W/ł | () | k-value kJ/m²-l | | A X k kJ/K |
| Doors | | , | | | 2.12 | _ | 1.6 | | 3.392 | $\stackrel{\prime}{\Box}$ | | | (26) |
| Windows Type | 1 | | | | 20.3 | x1. | /[1/(1.6)+ | 0.04] = | 30.53 | | | | (27) |
| Windows Type | 2 | | | | 4.55 | x1. | /[1/(1.6)+ | 0.04] = | 6.84 | = | | | (27) |
| Walls Type1 | 31.54 | 4 | 2.12 | \neg | 29.42 | 2 x | 0.13 | | 3.88 | | | | (29) |
| Walls Type2 | 2.28 | | 0 | = | 2.28 | × | 0.12 | = | 0.28 | - | | i i | (29) |
| Walls Type3 | 58.57 | 7 | 24.85 | <u> </u> | 33.72 | 2 x | 0.16 | <u> </u> | 5.4 | - | | i i | (29) |
| Total area of el | lements, | m² | | | 92.39 | | | | | | | | (31) |
| Party wall | | | | | 26.02 | 2 x | 0 | | 0 | | | | (32) |
| Party floor | | | | | 86.75 | <u> </u> | | | | | | i i | (32a) |
| Party ceiling | | | | | 86.75 | = | | | | _ | | 7 F | (32b) |
| * for windows and ** include the area | | | | | | ated using | formula 1 | /[(1/U-valu | ıe)+0.04] a | s given in | paragraph | 3.2 | `` |
| Fabric heat los | | | | o ama pan | | | (26)(30) |) + (32) = | | | | 50.32 | (33) |
| Heat capacity (| · | , | , | | | | | ((28) | .(30) + (32 | 2) + (32a). | (32e) = | 11168.60 | |
| Thermal mass | paramet | er (TMF | P = Cm ÷ | TFA) ir | ı kJ/m²K | | | Indica | tive Value: | Low | | 100 | (35) |
| For design assess can be used instea | | | | constructi | ion are not | t known pr | ecisely the | e indicative | values of | TMP in Ta | able 1f | | |
| Thermal bridge | | | | ısing Ap | pendix ł | < | | | | | | 13.86 | (36) |
| if details of therma | , | , | | | • | | | | | | | | ` ′ |
| Total fabric hea | at loss | | | | | | | (33) + | (36) = | | | 64.18 | (37) |
| Ventilation hea | t loss ca | lculated | monthly | ′ | | | | (38)m | = 0.33 × (| 25)m x (5) | 1 | Ī | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |



| (38)m= | 45.78 | 44.79 | 44.79 | 42.99 | 41.91 | 41.41 | 40.93 | 40.93 | 42.17 | 42.99 | 43.86 | 44.79 | | (38) |
|---|------------------|-----------------------|-------------|--------------|--------------------|----------------------|-----------------------------|------------------------|---------------------|------------------------|------------------------|--------------------|---------|-------|
| Heat tr | ansfer c | coefficier | nt, W/K | | | | | | (39)m | = (37) + (3 | 38)m | | | |
| (39)m= | 109.96 | 108.97 | 108.97 | 107.17 | 106.09 | 105.59 | 105.11 | 105.11 | 106.35 | 107.17 | 108.04 | 108.97 | | |
| Heat Id | ss para | meter (H | HLP), W | /m²K | | | | | | Average = = (39)m ÷ | Sum(39) ₁ . | 12 /12= | 107.29 | (39) |
| (40)m= | 1.27 | 1.26 | 1.26 | 1.24 | 1.22 | 1.22 | 1.21 | 1.21 | 1.23 | 1.24 | 1.25 | 1.26 | | |
| Numbe | er of day | rs in moi | nth (Tab | le 1a) | • | • | • | | , | Average = | Sum(40) ₁ | 12 /12= | 1.24 | (40) |
| rannoc | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| (41)m= | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | (41) |
| (/ | | | | | | | | | | | | | | , , |
| 4. Wa | iter heat | ing ene | rgy requi | irement: | | | | | | | | kWh/ye | ear: | |
| ٨٥٥٠١٣٥ | ad agai | nanay l | NI. | | | | | | | | | | | (40) |
| | | ıpancy, l 9, N = 1 | | [1 - exp | (-0.0003 | 349 x (TF | A -13.9 |)2)] + 0.0 | 0013 x (| ΓFA -13. | | 58 | | (42) |
| | A £ 13.9 | • | | | | | | | | | | | | |
| | | | | | | | | (25 x N) to achieve | | se target o | | .44 | | (43) |
| | | - | | r day (all w | | - | - | | | g | | | | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| Hot water | er usage ii | n litres per | day for ea | ach month | Vd,m = fa | ctor from 7 | Table 1c x | | • | | ļ. | | | |
| (44)m= | 104.99 | 101.17 | 97.35 | 93.53 | 89.71 | 85.9 | 85.9 | 89.71 | 93.53 | 97.35 | 101.17 | 104.99 | | |
| | | | | ! | | | | | | | m(44) ₁₁₂ = | L | 1145.29 | (44) |
| Energy (| content of | hot water | used - cal | culated mo | onthly = 4. | 190 x Vd,r | n x nm x E | OTm / 3600 |) kWh/mor | nth (see Ta | ables 1b, 1 | c, 1d) | | |
| (45)m= | 156.06 | 136.49 | 140.85 | 122.8 | 117.83 | 101.67 | 94.22 | 108.11 | 109.41 | 127.5 | 139.18 | 151.14 | | _ |
| If instant | taneous w | ater heatii | ng at point | of use (no | hot water | storage), | enter 0 in | boxes (46) | | Fotal = Su | m(45) ₁₁₂ = | = [| 1505.25 | (45) |
| (46)m= | 23.41 storage | 20.47 | 21.13 | 18.42 | 17.67 | 15.25 | 14.13 | 16.22 | 16.41 | 19.13 | 20.88 | 22.67 | | (46) |
| | • | | clared lo | oss facto | r is knov | vn (kWh | /dav)· | | | | | 0 | | (47) |
| • | | | m Table | | | (| ,, , . | | | | | 0 | | (48) |
| • | | | | , kWh/y€ | ear | | | (47) x (48) |) = | | | 0 | | (49) |
| • | | | _ | nder loss | | s not kno | | () (-) | | | | <u> </u> | | (1.0) |
| Cylinde | er volum | ne (litres |) includir | ng any s | olar stor | age with | in same | : | | | 1 | 10 | | (50) |
| | - | _ | | dwelling, | | | | | (50) | | | | | |
| | | | • | | | | , | enter '0' in | box (50) | | | | | |
| | | Ū | | om Tabl | e 2 (kW | h/litre/da | ıy) | | | | 0. | 02 | | (51) |
| | | from Ta | | Oh | | | | | | | | .03 | | (52) |
| • | | | m Table | | | | | | | | 0 | .6 | | (53) |
| • | | | - | , kWh/ye | ear | | | ((50) x (51 |) x (52) x | (53) = | | 03 | | (54) |
| · | , , | 54) in (5 | • | for each | month | | | ((56)m = (| 55) ~ (44). | m | 1. | .03 | | (55) |
| | | | | | | 20.00 | | | | | 20.00 | 20.04 | | (50) |
| (56)m= | 32.01 | 28.92 | 32.01 | 30.98 | 32.01 m = (56)m | 30.98 x [(50) – (| 32.01 H11)1 <i>÷ (</i> 5 | 32.01 0) else (5 | 30.98 7)m = (56) | 32.01 m where (| 30.98 H11) is fro | 32.01 m Appendi | ix H | (56) |
| - | | | i | 1 | · · · | I | · · · · | | | | ī | · · · | A (1 | (EZ\ |
| (57)m= | 32.01 | 28.92 | 32.01 | 30.98 | 32.01 | 30.98 | 32.01 | 32.01 | 30.98 | 32.01 | 30.98 | 32.01 | | (57) |



| Primary circuit loss (annual) from Table 3 Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m | 360 | (58 | 8) |
|--|-------------------------|---------------|----|
| (modified by factor from Table H5 if there is solar water heating and a cylinder thermos | stat) | | |
| (59)m= 30.58 27.62 30.58 29.59 30.58 29.59 30.58 29.59 30.58 | 29.59 30.58 | (59 | 9) |
| Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m | | | |
| (61)m= 0 0 0 0 0 0 0 0 0 | 0 0 | (61 | 1) |
| Total heat required for water heating calculated for each month $(62)m = 0.85 \times (45)m + (62)m $ | (46)m + (57)m + | (59)m + (61)m | |
| (62)m= 218.65 193.03 203.44 183.37 180.41 162.24 156.81 170.7 169.98 190.09 | 199.75 213.73 | (62 | 2) |
| Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution | on to water heating) | | |
| (add additional lines if FGHRS and/or WWHRS applies, see Appendix G) | | | |
| (63)m= 0 0 0 0 0 0 0 0 0 0 | 0 0 | (63 | 3) |
| Output from water heater | | | |
| (64)m= 218.65 193.03 203.44 183.37 180.41 162.24 156.81 170.7 169.98 190.09 | 199.75 213.73 | | |
| Output from water heater | (annual) ₁₁₂ | 2242.2 (64 | 4) |
| Heat gains from water heating, kWh/month 0.25 x $[0.85 \times (45)\text{m} + (61)\text{m}] + 0.8 \text{ x} [(46)\text{m}]$ | + (57)m + (59)m | 1] | |
| (65)m= 101.96 90.61 96.9 89.29 89.25 82.26 81.4 86.02 84.83 92.47 | 94.73 100.33 | (65 | 5) |
| include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from | om community h | eating | |
| 5. Internal gains (see Table 5 and 5a): | • | | |
| Metabolic gains (Table 5), Watts | | | |
| Jan Feb Mar Apr May Jun Jul Aug Sep Oct | Nov Dec | | |
| (66)m= 154.71 154.71 154.71 154.71 154.71 154.71 154.71 154.71 154.71 154.71 | 154.71 154.71 | (66 | 6) |
| Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5 | | | |
| (67)m= 51.92 46.12 37.51 28.39 21.22 17.92 19.36 25.17 33.78 42.89 | 50.06 53.37 | (67 | 7) |
| Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5 | • | | |
| (68)m= 347.72 351.32 342.23 322.88 298.44 275.48 260.13 256.52 265.62 284.97 | 309.41 332.37 | (68 | 8) |
| Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5 | I | • | |
| (69)m= 53.05 53.05 53.05 53.05 53.05 53.05 53.05 53.05 53.05 | 53.05 53.05 | (69 | 9) |
| Pumps and fans gains (Table 5a) | | 1 | |
| (70)m= 0 0 0 0 0 0 0 0 0 0 | 0 0 | (70 | 0) |
| Losses e.g. evaporation (negative values) (Table 5) | | 1 | |
| (71)m= -103.14 | -103.14 -103.14 | (71 | 1) |
| Water heating gains (Table 5) | l l | | |
| (72)m= 137.05 134.84 130.25 124.01 119.96 114.25 109.41 115.62 117.82 124.28 | 131.57 134.85 | (72 | 2) |
| Total internal gains = $(66)m + (67)m + (68)m + (69)m + (70)m + (70)m$ | | ` | , |
| (73)m= 641.31 636.9 614.61 579.9 544.24 512.27 493.52 501.93 521.84 556.77 | 595.67 625.21 | (73 | 3) |
| 6. Solar gains: | 000.07 | | -, |
| Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable | le orientation. | | |
| Orientation: Access Factor Area Flux g_ | FF | Gains | |
| 0_ | able 6c | (VV) | |
| Northeast 0.9x 0.77 x 20.3 x 11.51 x 0.63 x | 0.8 = | 81.61 (75 | 5) |
| Northeast 0.9x 0.77 x 20.3 x 23.55 x 0.63 x | 0.8 = | 167.01 (75 | 5) |
| | | | |



| Northeast _{0.9x} | 0.77 | X | 20 | .3 | x | 41.13 | X | 0.6 | 3 | _ x [| 0.8 | = | 291.6 | (75) |
|-----------------------------|------------|------------|------------|------------------|-------------------|----------------|----------|-----------|-------------|--------|---------------|----------|----------|------|
| Northeast _{0.9x} | 0.77 | Х | 20 | .3 | x | 67.8 | X | 0.6 | 3 | _ x [| 0.8 | = | 480.7 | (75) |
| Northeast _{0.9x} | 0.77 | X | 20 | .3 | x | 89.77 | X | 0.6 | 3 | x [| 0.8 | = | 636.46 | (75) |
| Northeast _{0.9x} | 0.77 | X | 20 | .3 | x | 97.5 | X | 0.6 | 3 | x [| 0.8 | = | 691.31 | (75) |
| Northeast _{0.9x} | 0.77 | X | 20 | .3 | x | 92.98 | X | 0.6 | 3 | _ x [| 0.8 | = | 659.24 | (75) |
| Northeast _{0.9x} | 0.77 | X | 20 | .3 | x | 75.42 | X | 0.6 | 3 | x [| 0.8 | = | 534.73 | (75) |
| Northeast 0.9x | 0.77 | X | 20 | .3 | x | 51.24 | X | 0.6 | 3 | x [| 0.8 | = | 363.34 | (75) |
| Northeast _{0.9x} | 0.77 | x | 20 | .3 | x | 29.6 | x | 0.6 | 3 | x | 0.8 | = | 209.86 | (75) |
| Northeast _{0.9x} | 0.77 | x | 20 | .3 | x | 14.52 | X | 0.6 | 3 | x | 0.8 | = | 102.99 | (75) |
| Northeast 0.9x | 0.77 | X | 20 | .3 | x | 9.36 | X | 0.6 | 3 | x [| 0.8 | = | 66.37 | (75) |
| Northwest 0.9x | 0.77 | х | 4.5 | 55 | x | 11.51 | X | 0.6 | 3 | x [| 0.8 | = | 18.29 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 23.55 | X | 0.6 | 3 | x [| 0.8 | = | 37.43 | (81) |
| Northwest 0.9x | 0.77 | Х | 4.5 | 55 | x | 41.13 | X | 0.6 | 3 | x [| 0.8 | = | 65.36 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 67.8 | X | 0.6 | 3 | x [| 0.8 | = | 107.74 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 89.77 | X | 0.6 | 3 | x [| 0.8 | = | 142.66 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 97.5 | X | 0.6 | 3 | x [| 0.8 | = | 154.95 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 92.98 | X | 0.6 | 3 | x | 0.8 | = | 147.76 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 75.42 | X | 0.6 | 3 | x [| 0.8 | = | 119.85 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 51.24 | X | 0.6 | 3 | x [| 0.8 | = | 81.44 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 29.6 | X | 0.6 | 3 | x [| 0.8 | = | 47.04 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 14.52 | X | 0.6 | 3 | x [| 0.8 | = | 23.08 | (81) |
| Northwest 0.9x | 0.77 | X | 4.5 | 55 | x | 9.36 | X | 0.6 | 3 | _ x [| 0.8 | = | 14.88 | (81) |
| | | | | | | | _ | | | | | | | _ |
| Solar gains in | watts, ca | alculated | for eac | h month | 1 | | (83)m | n = Sum(7 | '4)m | .(82)m | | | - | |
| (83)m= 99.9 | 204.44 | 356.96 | 588.45 | 779.12 | 846.20 | | 654 | .58 444 | 4.77 | 256.9 | 126.07 | 81.24 | | (83) |
| Total gains – i | nternal a | | | | | | | | | | | 1 | 7 | |
| (84)m= 741.21 | 841.34 | 971.56 | 1168.34 | 1323.36 | 1358.5 | 3 1300.53 | 1156 | 6.51 966 | 6.62 | 813.67 | 721.73 | 706.45 | | (84) |
| 7. Mean inter | rnal temp | erature | (heating | seasor | 1) | | | | | | | | | |
| Temperature | during h | eating p | eriods ir | the livi | ng area | a from Ta | ble 9 | , Th1 (° | C) | | | | 21 | (85) |
| Utilisation fac | ctor for g | ains for I | iving are | ea, h1,m | (see | able 9a) | , | | | | | | - | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | А | ug S | Sep | Oct | Nov | Dec | | |
| (86)m= 0.93 | 0.91 | 0.85 | 0.76 | 0.6 | 0.45 | 0.32 | 0.3 | 35 0 | .6 | 0.81 | 0.91 | 0.93 | | (86) |
| Mean_interna | al tempera | ature in | living are | ea T1 (f | ollow s | teps 3 to | 7 in T | able 9c | ;) | | | | _ | |
| (87)m= 18.78 | 19.05 | 19.57 | 20.13 | 20.63 | 20.87 | 20.96 | 20. | 95 20 | .73 | 20.13 | 19.29 | 18.83 | | (87) |
| Temperature | during h | eating p | eriods ir | rest of | dwellir | ng from Ta | able 9 | 9, Th2 (| °C) | | | | | |
| (88)m= 19.87 | 19.88 | 19.88 | 19.89 | 19.9 | 19.91 | 19.91 | 19. | | 9.9 | 19.89 | 19.89 | 19.88 |] | (88) |
| Utilisation fac | ctor for a | ains for i | rest of d | wellina | h2 m (| see Table | 9a) | | | | • | | - | |
| (89)m= 0.92 | 0.89 | 0.83 | 0.72 | 0.56 | 0.39 | 0.24 | 0.2 | 27 0. | 53 | 0.78 | 0.9 | 0.92 | 1 | (89) |
| Mean interna | l tompor | | | of dwall | ing To | | <u> </u> | ! | | 2 00/ | | <u> </u> | 1 | |
| (90)m= 16.95 | 17.35 | 18.08 | 18.86 | 19.51 | 19.8 | 19.89 | 19. | | .66 | 18.89 | 17.71 | 17.03 | 1 | (90) |
| (00)= | 1 | . 5.50 | . 5.50 | 1 | 1 .0.0 | 1 .0.00 | 1 '5. | 10 | | | ing area ÷ (4 | <u> </u> | 0.36 | (91) |
| | | | | | ` | - : | ,. | <i>c</i> | | | J | • | 0.00 | |
| Mean interna (92)m= 17.6 | l tempera | ature (fo | r the wh | ole dwe 19.91 | lling) = 20.18 | _ | + (1 | | ≺T2 0.04 | 19.33 | 18.27 | 17.67 | 1 | (92) |
| | | | | | | | | | | | | | | |



| Apply adjustment to the mean internal temperature from Table 4e, v | where appro | priate | | | | |
|--|----------------|--------------|------------|------------------------|-----------|-------------|
| (93)m= 17.6 17.96 18.61 19.31 19.91 20.18 20.27 20.2 | 27 20.04 | 19.33 | 18.27 | 17.67 | | (93) |
| 8. Space heating requirement | | | | | | |
| Set Ti to the mean internal temperature obtained at step 11 of Table | e 9b, so tha | t Ti,m=(| 76)m an | d re-calc | ulate | |
| the utilisation factor for gains using Table 9a Jan Feb Mar Apr May Jun Jul Au | ıg Sep | Oct | Nov | Dec | | |
| Utilisation factor for gains, hm: | ig Gep | Oct | INOV | Dec | | |
| (94)m= 0.89 0.87 0.8 0.7 0.56 0.4 0.27 0.3 | 0.54 | 0.75 | 0.87 | 0.9 | | (94) |
| Useful gains, hmGm , W = (94)m x (84)m | | | | | | |
| (95)m= 663.26 728.16 781.19 823.04 735.67 546.46 344.94 341. | 42 521.94 | 613.91 | 626.31 | 634.64 | | (95) |
| Monthly average external temperature from Table 8 | | | | | | |
| (96)m= 4.5 5 6.8 8.7 11.7 14.6 16.9 16. | | 10.8 | 7 | 4.9 | | (96) |
| Heat loss rate for mean internal temperature, Lm , W = $[(39)$ m x $[(93)$ m x | | 914.22 | 1217.97 | 1391.51 | | (97) |
| Space heating requirement for each month, kWh/month = $0.024 \times [0.00]$ | | | | 1391.31 | | (01) |
| (98)m= 578.32 459.48 376.68 226.09 100.36 0 0 0 | ì | 223.43 | 426 | 563.11 | | |
| | Total per year | (kWh/year |) = Sum(9 | 8) _{15,912} = | 2953.48 | (98) |
| Space heating requirement in kWh/m²/year | | | | | 34.05 | 」 (99) |
| 9b. Energy requirements – Community heating scheme | | | | | | |
| This part is used for space heating, space cooling or water heating p | rovided by | a commi | unity sch | neme. | | |
| Fraction of space heat from secondary/supplementary heating (Table | | | y | | 0 | (301) |
| Fraction of space heat from community system $1 - (301) =$ | | | | | 1 | (302) |
| The community scheme may obtain heat from several sources. The procedure allows | for CHP and t | up to four o | other heat | sources; ti | he latter | _ |
| includes boilers, heat pumps, geothermal and waste heat from power stations. See A | ppendix C. | | | ı | | ٦,,,,, |
| Fraction of heat from Community CHP | | | | | 0.6 | (303a) |
| Fraction of community heat from heat source 2 | | | | | 0.4 | (303b) |
| Fraction of total space heat from Community CHP | | (3) | 02) x (303 | a) = | 0.6 | (304a) |
| Fraction of total space heat from community heat source 2 | | (3 | 02) x (303 | b) = | 0.4 | (304b) |
| Factor for control and charging method (Table 4c(3)) for community | heating sys | tem | | | 1 | (305) |
| Distribution loss factor (Table 12c) for community heating system | | | | | 1.05 | (306) |
| Space heating | | | | | kWh/year | |
| Annual space heating requirement | | | | | 2953.48 | 7 |
| Space heat from Community CHP | (98) x (30 | 04a) x (305 | 5) x (306) | = | 1860.69 | ☐ (307a) |
| Space heat from heat source 2 | (98) x (30 | 04b) x (305 | 5) x (306) | ! _ | 1240.46 |] (307b) |
| · | , , , | , , | , , , | | | ╡` |
| Efficiency of secondary/supplementary heating system in % (from Ta | | | , | | 0 | (308 |
| Space heating requirement from secondary/supplementary system | (98) x (30 | 01) x 100 ÷ | ÷ (308) = | | 0 | (309) |
| Water heating | | | | i | | _ |
| Annual water heating requirement | | | | | 2242.2 | ╛ |
| If DHW from community scheme: Water heat from Community CHP | (64) x (3(| 03a) x (305 | 5) x (306) | <u> </u> | 1412.58 | (310a) |
| Tate. Heat from Community Of II | (0.) x (00 | . Ju, n (000 | , (000) | | 1412.00 | ارنانانان |



| Water heat from heat source 2 | | (64) x (303b) x (305) x (306) = | 941.72 (310 |
|---|--|---|--------------------------|
| Electricity used for heat distribution | | 0.01 × [(307a)(307e) + (310a)(310e)] = | 54.55 (313 |
| Cooling System Energy Efficiency | Ratio | | 0 (314 |
| Space cooling (if there is a fixed co | oling system, if not enter 0) | = (107) ÷ (314) = | 0 (315 |
| Electricity for pumps and fans withi mechanical ventilation - balanced, | | ıtside | 0 (330 |
| warm air heating system fans | oxudot of poolaro input from ot | atoliu o | 0 (330 |
| pump for solar water heating | | | 0 (330 |
| Total electricity for the above, kWh | /vear | =(330a) + (330b) + (330g) = | 0 (331 |
| Energy for lighting (calculated in Ap | | , , , , , , | 366.79 (332 |
| Electricity generated by PVs (Appe | | | -156.1 (333 |
| Electricity generated by wind turbin | e (Appendix M) (negative quan | ntity) | 0 (334 |
| 10b. Fuel costs – Community hea | ting scheme | | |
| | Fuel kWh/year | Fuel Price (Table 12) | Fuel Cost £/year |
| Space heating from CHP | (307a) x | 2.65 x 0.01 = | 49.31 (340 |
| Space heating from heat source 2 | (307b) x | 3.78 x 0.01 = | 46.89 (340 |
| Water heating from CHP | (310a) x | 2.65 x 0.01 = | 37.43 (342 |
| Water heating from heat source 2 | (310b) x | 3.78 x 0.01 = | 35.6 (342 |
| | | Fuel Price | |
| Pumps and fans | (331) | 11.46 × 0.01 = | 0 (349 |
| Energy for lighting | (332) | 11.46 x 0.01 = | 42.03 (350 |
| Additional standing charges (Table | 12) | | 106 (351 |
| Energy saving/generation technolo Item 1 | gies | 11.46 x 0.01 = | -17.89 (352 |
| Total energy cost | = (340a)(342e) + (345)(354 | 4) = | 299.37 (355 |
| 11b. SAP rating - Community hea | ting scheme | | |
| Energy cost deflator (Table 12) | | | 0.47 (356 |
| Energy cost factor (ECF) | $[(355) \times (356)] \div [(4) + 45.0] =$ | | 1.07 (357 |
| SAP rating (section12) | | | 85.1 (358 |
| 12b. CO2 Emissions – Community | heating scheme | | |
| Electrical efficiency of CHP unit | | | 25.58 (361 |
| Heat efficiency of CHP unit | | | 58.32 (362 |
| | | Energy Emission factor kWh/year kg CO2/kWh | Emissions kg CO2/year |
| Space heating from CHP) | (307a) × 100 ÷ (362) = | 3190.45 X 0.2 | 631.71 (363 |
| less credit emissions for electricity | -(307a) × (361) ÷ (362) = | 816.09 × 0.53 | -431.71 (364 |



| Water heated by CHP | (310a) × 100 ÷ (362) = | 2422.1 × | 0.2 |] | 479.57 | (365) |
|---|--|--|---|-------------------|---|--|
| less credit emissions for electricity | $-(310a) \times (361) \div (362) =$ | 619.55 × | 0.53 |] | -327.74 | (366) |
| Efficiency of heat source 2 (%) | If there is CHP us | sing two fuels repeat (363) to | o (366) for the secon | nd fuel | 92 | (367b) |
| CO2 associated with heat source 2 | [(307) | o)+(310b)] x 100 ÷ (367b) x | 0.2 | = | 469.64 | (368) |
| Electrical energy for heat distribution | on | [(313) x | 0.52 | = | 28.2 | (372) |
| Total CO2 associated with commun | nity systems | (363)(366) + (368)(3 | 72) | = | 849.67 | (373) |
| CO2 associated with space heating | g (secondary) | (309) x | 0 | = | 0 | (374) |
| CO2 associated with water from im | mersion heater or instanta | neous heater (312) x | 0.2 | = | 0 | (375) |
| Total CO2 associated with space a | nd water heating | (373) + (374) + (375) = | | | 849.67 | (376) |
| CO2 associated with electricity for | pumps and fans within dwe | elling (331)) x | 0.52 | = | 0 | (378) |
| CO2 associated with electricity for | lighting | (332))) x | 0.52 |] = | 189.63 | (379) |
| Energy saving/generation technolo | gies (333) to (334) as appl | licable | | | | 7 |
| Item 1 | (0-0) | | 0.53 × 0. | 01 = | -82.58 | <u> </u> (380) |
| Total CO2, kg/year | sum of (376)(382) = | | | | 956.73 | (383) |
| Dwelling CO2 Emission Rate | te (383) ÷ (4) = | | | Ļ | 11.03 | (384) |
| El rating (section 14) | hoating sohomo | | | | 90.27 | (385) |
| 13b. Primary Energy – Community Electrical efficiency of CHP unit | nealing scheme | | | | 25.58 | (361) |
| | | | | | | |
| Heat efficiency of CHP unit | | | | | | 」 |
| Heat efficiency of CHP unit | | Energy | Primary | | 58.32 | (362) |
| Heat efficiency of CHP unit | | Energy kWh/year | Primary factor | | | (362) |
| Heat efficiency of CHP unit Space heating from CHP) | (307a) × 100 ÷ (362) = | • | - | | 58.32 Energy | (362) |
| · | (307a) × 100 ÷ (362) = -(307a) × (361) ÷ (362) = | kWh/year | factor | | 58.32 Energy Wh/year | _ |
| Space heating from CHP) | | kWh/year x | factor | | 58.32 Energy Wh/year 3254.25 | (363) |
| Space heating from CHP) less credit emissions for electricity | $-(307a) \times (361) \div (362) =$ | kWh/year 3190.45 | 1.02 2.92 | | 58.32 Energy Wh/year 3254.25 -2382.99 | (363) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP | $-(307a) \times (361) \div (362) =$ $(310a) \times 100 \div (362) =$ $-(310a) \times (361) \div (362) =$ | kWh/year 3190.45 X 816.09 X 2422.1 X | 1.02 2.92 1.02 2.92 | kv]]] | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 | (363) (364) (365) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity | $-(307a) \times (361) \div (362) =$ $(310a) \times 100 \div (362) =$ $-(310a) \times (361) \div (362) =$ If there is CHP us | kWh/year 3190.45 X 816.09 X 2422.1 X 619.55 X | 1.02 2.92 1.02 2.92 | kv]]] | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 | (363) (364) (365) (366) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) | $-(307a) \times (361) \div (362) =$ $(310a) \times 100 \div (362) =$ $-(310a) \times (361) \div (362) =$ If there is CHP us $= 2$ [(307b) | 3190.45 X 816.09 X 2422.1 X 619.55 X sing two fuels repeat (363) to | 1.02 2.92 1.02 2.92 0 (366) for the second | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 | (363) (364) (365) (366) (367b) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source | $-(307a) \times (361) \div (362) =$ $(310a) \times 100 \div (362) =$ $-(310a) \times (361) \div (362) =$ If there is CHP use 2 [(307b) | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the second 1.02 | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 | (363) (364) (365) (366) (367b) (368) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP use 2 [(307b) nunity systems | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 | (363) (364) (365) (366) (367b) (368) (372) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with comme | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP use 2 [(307b) nunity systems (unless specified otherwise | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 | (363) (364) (365) (366) (367b) (368) (372) (373) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with commits if it is negative set (373) to zero | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP use 2 [(307b) nunity systems (unless specified otherwise ing (secondary) | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 72) | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 4111.38 | (363) (364) (365) (366) (367b) (368) (372) (373) (373) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with commits if it is negative set (373) to zero (373) to zero (373) to zero (373) associated with space heat | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP use 2 [(307b) on nunity systems (unless specified otherwise) ing (secondary) immersion heater or instar | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 72) C) | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 4111.38 | (363) (364) (365) (366) (367b) (368) (372) (373) (373) (374) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with commitie it is negative set (373) to zero (373) to zero (373) to zero (373) associated with space heatenergy associated with water from | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP use 2 [(307b) nunity systems (unless specified otherwise ing (secondary) immersion heater or instart and water heating | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 72) C) | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 0 0 | (363) (364) (365) (366) (367b) (368) (372) (373) (373) (374) (375) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with common if it is negative set (373) to zero (373) to zero (373) to zero (373) associated with space heated Energy associated with water from Total Energy associated with space | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP uses 2 [(307b) nunity systems (unless specified otherwise ing (secondary) immersion heater or instance and water heating ing | kWh/year 3190.45 | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 C) 0 1.02 2.92 | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 0 0 4111.38 | (363) (364) (365) (366) (367b) (368) (372) (373) (373) (374) (375) (376) |
| Space heating from CHP) less credit emissions for electricity Water heated by CHP less credit emissions for electricity Efficiency of heat source 2 (%) Energy associated with heat source Electrical energy for heat distribution Total Energy associated with common if it is negative set (373) to zero in Energy associated with space heat Energy associated with water from Total Energy associated with space Energy associated with space cool | -(307a) × (361) ÷ (362) = (310a) × 100 ÷ (362) = -(310a) × (361) ÷ (362) = If there is CHP uses a company of the company of | kWh/year 3190.45 816.09 2422.1 619.55 x sing two fuels repeat (363) to b)+(310b)] × 100 ÷ (367b) × [(313) × (363)(366) + (368)(376) × (309) × ntaneous heater(312) × (373) + (374) + (375) = (315) × | 1.02 2.92 1.02 2.92 0 (366) for the secon 1.02 C) 0 1.02 2.92 | kV | 58.32 Energy Wh/year 3254.25 -2382.99 2470.54 -1809.1 92 2419.38 159.3 4111.38 0 0 4111.38 0 | (363) (364) (365) (366) (367b) (368) (372) (373) (373) (374) (375) (376) (377) |



Energy saving/generation technologies Item 1

Total Primary Energy, kWh/year

sum of (376)...(382) =

2.92 x 0.01 = -455.82 (380)

4726.6 (383)

SAP 2009 Overheating Assessment



Calculated by Stroma FSAP 2009 program, produced and printed on 17 April 2015

Property Details: 07-14-40586 B17 PL1

Dwelling type:FlatLocated in:EnglandRegion:Thames valley

Cross ventilation possible: No **Number of storeys:** 1

Front of dwelling faces: South West

Overshading: Average or unknown

Overhangs: None

Thermal mass parameter: Indicative Value Low

Night ventilation: False

Blinds, curtains, shutters: Light-coloured curtain or roller blind

Ventilation rate during hot weather (ach): 4 (Windows fully open)

Overheating Details:

Summer ventilation heat loss coefficient: 293.15 (P1)

Transmission heat loss coefficient: 64.2

Summer heat loss coefficient: 357.33 (P2)

Overhangs:

Orientation: Ratio: Z_overhangs:

North East (Rear Elev) 0 1 North West (Side Elev) 0 1

Solar shading:

| Orientation: | Z blinds: | Solar access: | Overnangs: | Z summer: | |
|------------------------|-----------|---------------|------------|-----------|------|
| North East (Rear Elev) | 0.6 | 0.9 | 1 | 0.54 | (P8) |
| North West (Side Elev) | 0.6 | 0.9 | 1 | 0.54 | (P8) |

Solar gains:

| Orientation | | Area | Flux | \mathbf{g}_{-} | FF | Shading | Gains |
|------------------------|-------|------|-------|------------------|-----|---------|-----------------------|
| North East (Rear Elev) | 0.9 x | 20.3 | 98.96 | 0.63 | 0.8 | 0.54 | 492.05 |
| North West (Side Elev) | 0.9 x | 4.55 | 98.96 | 0.63 | 0.8 | 0.54 | 110.29 |
| | | | | | | Total | 602.34 (P3/P4) |

Internal dains:

| | June | July | August | |
|--|-----------------|---------|--------|------|
| Internal gains | 512.27 | 493.52 | 501.93 | |
| Total summer gains | 1152.17 | 1095.86 | 1002.1 | (P5) |
| Summer gain/loss ratio | 3.22 | 3.07 | 2.8 | (P6) |
| Mean summer external temperature (Thames valley) | 15.4 | 17.8 | 17.8 | |
| Thermal mass temperature increment | 1.3 | 1.3 | 1.3 | |
| Threshold temperature | 19.92 | 22.17 | 21.9 | (P7) |
| Likelihood of high internal temperature | Not significant | Medium | Slight | |

Assessment of likelihood of high internal temperature: Medium

Predicted Energy Assessment



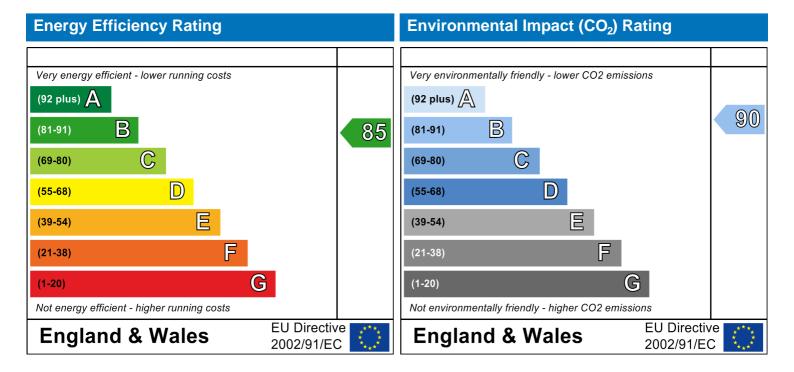
Flat B17

Dwelling type:
Date of assessment:
Produced by:
Total floor area:

Mid floor Flat
16 April 2015
Aymon Winter
86.75 m²

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2009 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbonn dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

Code for Sustainable Homes Report



Assessor and House Details

Assessor Name: Aymon Winter Assessor Number: STRO014511

Property Address: Flat B17

Buiding regulation assessment

kg/m²/year

TER 15.98 DER 11.84

The following code calculations are taken from the Code for Sustainable Homes Technical Guide (Nov 10)

Ene 1 Assessment - Dwelling Emission Rate

Total Energy Type CO2 Emissions for Codes Levels 1 - 5

| | % | kg/m²/year | |
|--|------|------------|-------|
| DER from SAP 2009 DER Worksheet | | 11.84 | (ZC1) |
| TER | | 15.98 | |
| Residual CO2 emissions offset from biofuel CHP | | 0 | (ZC5) |
| CO2 emissions offset from additional allowable electricty generation | | 0 | (ZC7) |
| Total CO2 emissions offset from SAP Section 16 allowances | | 0 | |
| DER accounting for SAP Section 16 allowances | | 11.84 | |
| % improvement DER/TER | 25.9 | | |

Total Energy Type CO2 Emissions for Codes Levels 6

| | kg/m²/year | |
|---|------------|-------|
| DER accounting for SAP Section 16 allowances | 11.84 | (ZC1) |
| CO2 emissions from appliances, equation (L14) | 15.85 | (ZC2) |
| CO2 emissions from cooking, equation (L16) | 2.09 | (ZC3) |
| Net CO2 emissions | 29.8 | (ZC8) |

Result:

Credits awarded for Ene 1 = 3.1

Code Level = 4

Ene 2 - Fabric energy Efficiency

Fabric energy Efficiency: 49.67 Credits awarded for Ene 2 = 0

Ene 7 - Low or Zero Carbon (LZC) Technologies

Reduction in CO2 Emissions

| | % | kg/m²/year | |
|-----------------------------|---|------------|--|
| Standard Case CO2 emissions | | 36.88 | |
| Standard DER | | 18.94 | |
| Actual Case CO2 emissions | | 29.78 | |
| Actual DER | | 11.84 | |

Reduction in CO2 emissions 19.25

Credits awarded for Ene 7 = 2

Technologies eligible to contribute to achieving the requirements of this issue must produce energy from renewable sources and meet all other ancillary requirements as defined by Directive 2009/28/EC of the European Parliament and of the Council of 23 April 2009 on the promotion of the use of energy from renewable sources and amending and subsequently repealing Directives 2001/77/EC and 2003/30/EC.

The following requirements must also be met:

- · Where not provided by accredited external renewables there must be a direct supply of energy produced to the dwelling under assessment.
- · Where covered by the Microgeneration Certification Scheme (MCS), technologies under 50kWe or 300kWth must be certified
- · Combined Heat and Power (CHP) schemes above 50kWe must be certified under the CHPQA standard.
- All technologies must be accounted for by SAP.

CHP schemes fuelled by mains gas are eligible to contribute to performance against this issue. Where these schemes are above 50kWe they must be certified under the CHPQA.

It is the responsibly of the Accredited OCDEA and Code Assessor to ensure all technologies use in the calculation are appropriate before awarding credits.